



# Robot Dynamics (Spill over!)

METR 4202: Advanced Control & **Robotics**

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# Robot Dynamics

## Dynamics



- For Manipulators, the general form is

$$\tau = M(\Theta)\ddot{\Theta} + V(\Theta, \dot{\Theta}) + G(\Theta)$$

where

- $\tau$  is a vector of joint torques
- $\Theta$  is the  $n \times 1$  vector of joint angles
- $M(\Theta)$  is the  $n \times n$  mass matrix
- $V(\Theta, \dot{\Theta})$  is the  $n \times 1$  vector of centrifugal and Coriolis terms
- $G(\Theta)$  is an  $n \times 1$  vector of gravity terms
- Notice that all of these terms depend on  $\Theta$  so the dynamics varies as the manipulator move



## Dynamics: Inertia

- The moment of inertia (second moment) of a rigid body B relative to a line L that passes through a reference point O and is parallel to a unit vector  $\mathbf{u}$  is given by:

$$I_u^O = \int_V \mathbf{p} \times (\mathbf{u} \times \mathbf{p}) \rho dV$$

$$= \int_V [p^2 \mathbf{u} - (\mathbf{p}^T \mathbf{u}) \mathbf{p}] \rho dV$$

- The scalar product of  $I_u^O$  with a second axis ( $\mathbf{w}$ ) is called the product of inertia

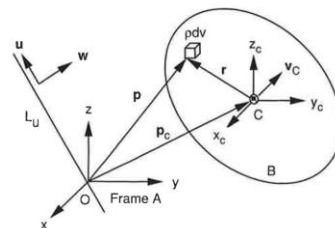
$$I_{uw}^O = I_u^O \cdot \mathbf{w} = \int_V [(u^T \mathbf{w}) p^2 - (\mathbf{p}^T \mathbf{u}) (\mathbf{p}^T \mathbf{w})] \rho dV$$

- If  $\mathbf{u}=\mathbf{w}$ , then we get the moment of inertia:

$$I_{uu} = \int_V [p^2 - (\mathbf{p}^T \mathbf{u})^2] \rho dV = m r_g^2$$

Where:  $\mathbf{r}_g$ : radius of gyration of B w/r/t to L

$$r_g = p^2 - (\mathbf{p}^T \mathbf{u})^2 = (\mathbf{u} \times \mathbf{p})^2$$



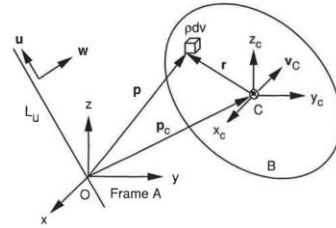
## Dynamics: Mass Matrix & Inertia Matrix

- This can be written in a Matrix form as:

$$I_u^O = I_B^O u$$

- Where  $I_B^O$  is the inertial matrix or inertial tensor of the body B about a reference point O

$$I_B^O = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yz} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}$$



- Where to get  $I_{xx}$ , etc? → Parallel Axis Theorem

If CM is the center of mass, then:

$$\begin{aligned} I_{xx}^O &= I_{xx}^{CM} + m(y_c^2 + z_c^2) & I_{xy}^O &= I_{xx}^{CM} + m x_c y_c \\ I_{yy}^O &= I_{yy}^{CM} + m(x_c^2 + z_c^2) & I_{yz}^O &= I_{xx}^{CM} + m y_c z_c \\ I_{zz}^O &= I_{zz}^{CM} + m(x_c^2 + y_c^2) & I_{zx}^O &= I_{xx}^{CM} + m z_c x_c \end{aligned}$$



## Dynamics: Mass Matrix

- The Mass Matrix: Determining via the Jacobian!

$$K = \sum_{i=1}^N K_i$$

$$K_i = \frac{1}{2} (m_i v_{C_i}^T v_{C_i} + \omega_i^T I_{C_i} \omega_i)$$

$$v_{C_i} = J_{v_i} \dot{\theta} \quad J_{v_i} = \begin{bmatrix} \frac{\partial p_{C_1}}{\partial \theta_1} & \cdots & \frac{\partial p_{C_i}}{\partial \theta_i} & \underbrace{0}_{i+1} & \cdots & \underbrace{0}_n \end{bmatrix}$$

$$\omega_i = J_{\omega_i} \dot{\theta} \quad J_{\omega_i} = \begin{bmatrix} \bar{\epsilon}_1 Z_1 & \cdots & \bar{\epsilon}_i Z_i & \underbrace{0}_{i+1} & \cdots & \underbrace{0}_n \end{bmatrix}$$

$$\therefore M = \sum_{i=1}^N (m_i J_{v_i}^T J_{v_i} + J_{\omega_i}^T I_{C_i} J_{\omega_i})$$

! M is symmetric, positive definite  $\therefore m_{ij} = m_{ji}, \dot{\theta}^T M \dot{\theta} > 0$



## Dynamics – Langrangian Mechanics

- Alternatively, we can use Langrangian Mechanics to compute the dynamics of a manipulator (or other robotic system)
- The Langrangian is defined as the difference between the Kinetic and Potential energy in the system
- Using this formulation and the concept of virtual work we can find the forces and torques acting on the system.
- This may seem more involved but is often easier to formulate for complex systems

$$L = K - P$$

$$\mathbf{F} = \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\mathbf{x}}} \right) - \frac{\partial L}{\partial \mathbf{x}}$$

$$\tau = \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta}$$



## Dynamics – Langrangian Mechanics [2]



$L = K - P$ ,  $\dot{\theta}$ : Generalized Velocities,  $M$ : Mass Matrix

$$\tau = \sum_{i=1}^N \tau_i = \frac{d}{dt} \left( \frac{\partial K}{\partial \dot{\theta}} \right) - \frac{\partial K}{\partial \theta} + \frac{\partial P}{\partial \theta}$$

$$K = \frac{1}{2} \dot{\theta}^T M(\theta) \dot{\theta}$$

$$\frac{d}{dt} \left( \frac{\partial K}{\partial \dot{\theta}} \right) = \frac{d}{dt} \left( \frac{\partial}{\partial \dot{\theta}} \left( \frac{1}{2} \dot{\theta}^T M(\theta) \dot{\theta} \right) \right) = \frac{d}{dt} (M \dot{\theta}) = M \ddot{\theta} + \dot{M} \dot{\theta}$$

$$\rightarrow \frac{d}{dt} \left( \frac{\partial K}{\partial \dot{\theta}} \right) - \frac{\partial K}{\partial \theta} = [M \ddot{\theta} + \dot{M} \dot{\theta}] - \left[ \frac{1}{2} \dot{\theta}^T \frac{\partial M}{\partial \theta} \dot{\theta} \right] = M \ddot{\theta} + \underbrace{\dot{M} \dot{\theta} - \frac{1}{2} \left[ \frac{\partial}{\partial \theta} \left( \dot{\theta}^T M \dot{\theta} \right) \right]}_{\mathbf{v}(\theta, \dot{\theta})}$$

$$\mathbf{v}(\theta, \dot{\theta}) = \underbrace{C(\theta) [\dot{\theta}^2]}_{\text{Centrifugal}} + \underbrace{B(\theta) [\dot{\theta} \dot{\theta}]}_{\text{Coriolis}}$$

$$\Rightarrow \tau = M(\theta) \ddot{\theta} + \mathbf{v}(\theta, \dot{\theta}) + \mathbf{g}(\theta)$$



## Dynamics – Langrangian Mechanics [3]

- The Mass Matrix: Determining via the Jacobian!

$$K = \sum_{i=1}^N K_i$$

$$K_i = \frac{1}{2} (m_i v_{C_i}^T v_{C_i} + \omega_i^T I_{C_i} \omega_i)$$

$$v_{C_i} = \mathbf{J}_{v_i} \dot{\theta} \quad \mathbf{J}_{v_i} = \begin{bmatrix} \frac{\partial \mathbf{p}_{C_1}}{\partial \theta_1} & \cdots & \frac{\partial \mathbf{p}_{C_i}}{\partial \theta_i} & \underbrace{0}_{i+1} & \cdots & \underbrace{0}_n \end{bmatrix}$$

$$\omega_i = \mathbf{J}_{\omega_i} \dot{\theta} \quad \mathbf{J}_{\omega_i} = \begin{bmatrix} \bar{\varepsilon}_1 Z_1 & \cdots & \bar{\varepsilon}_i Z_i & \underbrace{0}_{i+1} & \cdots & \underbrace{0}_n \end{bmatrix}$$

$$\therefore M = \sum_{i=1}^N (m_i \mathbf{J}_{v_i}^T \mathbf{J}_{v_i} + \mathbf{J}_{\omega_i}^T I_{C_i} \mathbf{J}_{\omega_i})$$

! M is symmetric, positive definite  $\therefore m_{ij} = m_{ji}, \dot{\theta}^T M \dot{\theta} > 0$



## Generalized Coordinates

- A significant feature of the Lagrangian Formulation is that any convenient coordinates can be used to derive the system.
- Go from Joint  $\rightarrow$  Generalized

– Define  $\mathbf{p}$ :  $d\mathbf{p} = \mathbf{J}d\mathbf{q}$

$$\mathbf{q} = [q_1 \quad \cdots \quad q_n] \rightarrow \mathbf{p} = [p_1 \quad \cdots \quad p_n]$$

$\rightarrow$  Thus: the kinetic energy and gravity terms become

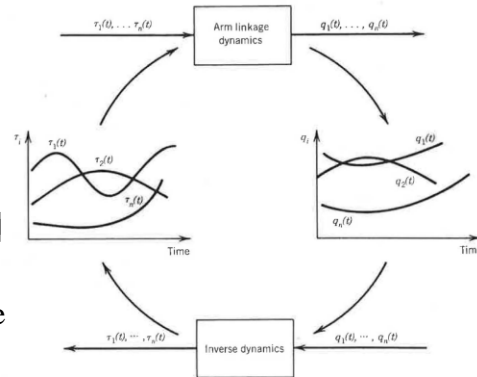
$$KE = \frac{1}{2} \dot{\mathbf{p}}^T \mathbf{H}^* \dot{\mathbf{p}} \quad \mathbf{G}^* = (\mathbf{J}^{-1})^T \mathbf{G}$$

$$\text{where: } \mathbf{H}^* = (\mathbf{J}^{-1})^T \mathbf{H} \mathbf{J}^{-1}$$



## Inverse Dynamics

- Forward dynamics governs the dynamic responses of a manipulator arm to the input torques generated by the actuators.
- The inverse problem:
  - Going from joint angles to torques
  - Inputs are desired trajectories described as functions of time  
 $\mathbf{q} = [q_1 \ \dots \ q_n] \rightarrow [\theta_1(t) \ \theta_2(t) \ \theta_3(t)]$
  - Outputs are joint torques to be applied at each instance  
 $\boldsymbol{\tau} = [\tau_1 \ \dots \ \tau_n]$
- Computation “big” (6DOF arm: 66,271 multiplications), but not scary (4.5 ms on PDP11/45)



Graphic from Asada & Slotinep. 119

## Also: Inverse Jacobian

- In many instances, we are also interested in computing the set of joint velocities that will yield a particular velocity at the end effector

$$\dot{\theta} = \mathbf{J}(\theta)^{-1} \dot{\mathbf{X}}$$

- We must be aware, however, that the inverse of the Jacobian may be undefined or singular. The points in the workspace at which the Jacobian is undefined are the *singularities* of the mechanism.
- Singularities typically occur at the workspace boundaries or at interior points where degrees of freedom are lost

## Inverse Jacobian Example

- For a simple two link RR manipulator:

$$x = L_1 \cos \theta_1 + L_2 \cos (\theta_1 + \theta_2)$$

$$y = L_1 \sin \theta_1 + L_2 \sin (\theta_1 + \theta_2)$$

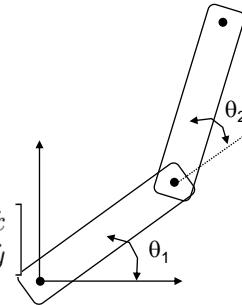
- The Jacobian for this is

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -L_1 s_1 - L_2 s_{12} & -L_2 s_{12} \\ L_1 c_1 + L_2 c_{12} & L_2 c_{12} \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

- Taking the inverse of the Jacobian yields

$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \frac{1}{L_1 L_2 s_2} \begin{bmatrix} L_2 c_{12} & L_2 s_{12} \\ -L_1 c_1 - L_2 c_{12} & -L_1 s_1 - L_2 s_{12} \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}$$

- Clearly, as  $\theta_2$  approaches 0 or  $\pi$  this manipulator becomes singular



## Static Forces

- We can also use the Jacobian to compute the joint torques required to maintain a particular force at the end effector

- Consider the concept of virtual work

$$F \cdot \delta \mathbf{X} = \tau \cdot \delta \theta$$

- Or

$$F^T \delta \mathbf{X} = \tau^T \delta \theta$$

- Earlier we saw that

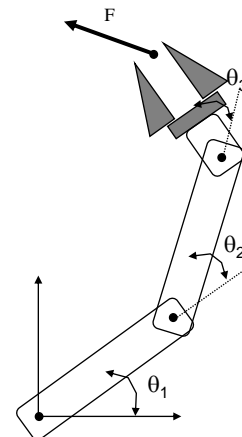
$$\delta \mathbf{X} = \mathbf{J} \delta \theta$$

- So that

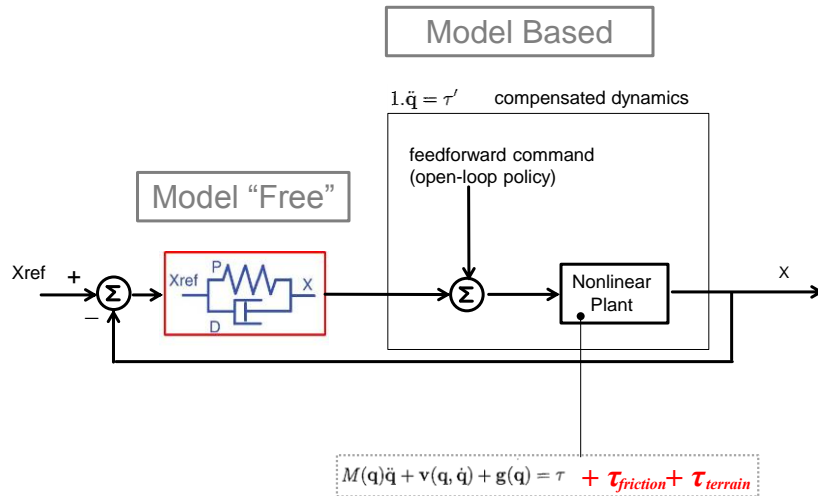
$$F^T \mathbf{J} = \tau^T$$

- Or

$$\tau = \mathbf{J}^T F$$



## Operation Space (Computed Torque)

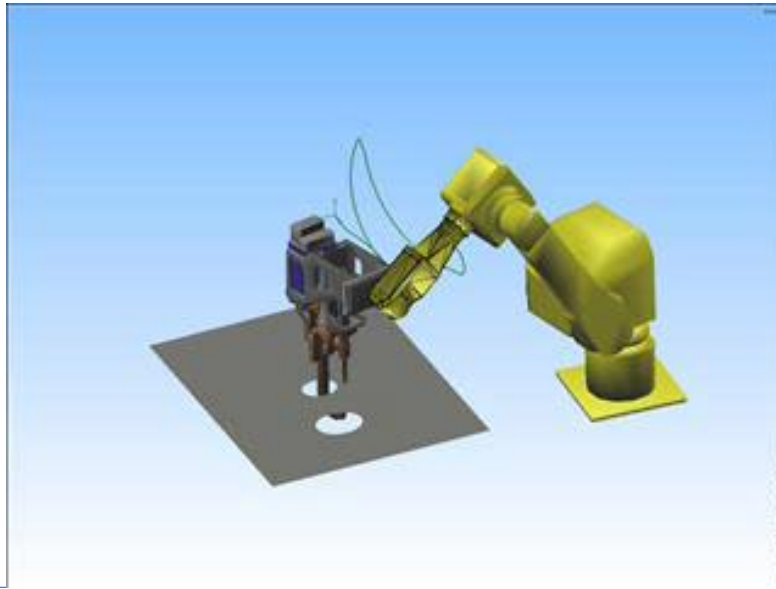


## Compensated Manipulation



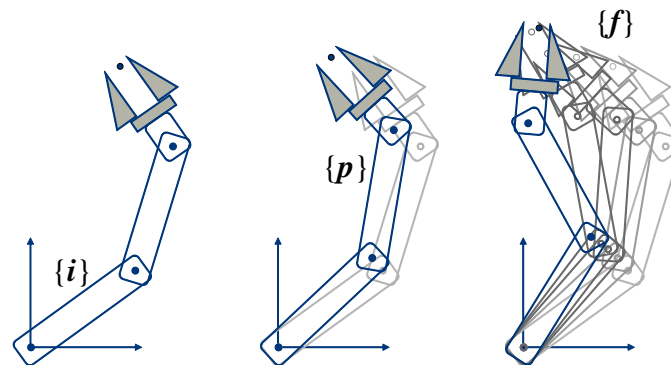


## Trajectory Generation & Planning



## Trajectory Generation

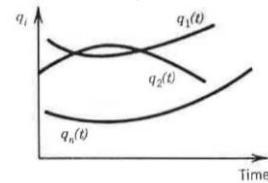
- The goal is to get from an initial position  $\{i\}$  to a final position  $\{f\}$  via a path points  $\{p\}$



## Joint Space

Consider only the **joint positions** as a function of time

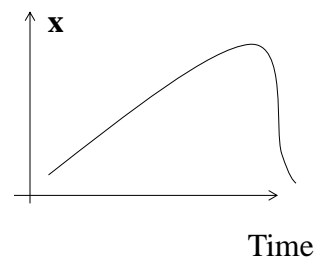
- + Since we control the joints, this is more direct
- -- If we want to follow a particular trajectory, not easy
  - at best lots of intermediate points
  - No guarantee that you can solve the Inverse Kinematics for all path points



## Cartesian Workspace

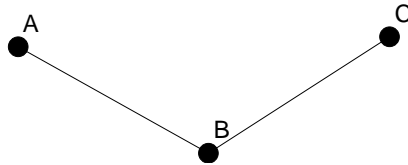
Consider the **Cartesian positions** as a function of time

- + Can track shapes exactly
- -- We need to solve the inverse kinematics and dynamics

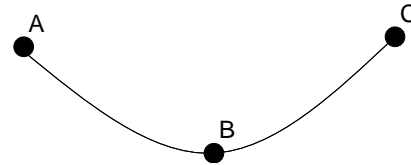


## Polynomial Trajectories

- Straight line Trajectories
- Polynomial Trajectories



- Simpler



$$u(t) = a_0 + a_1t + a_2t^2 + a_3t^3$$

- Parabolic blends are smoother
- Use “pseudo via points”



## Summary

- Kinematics is the study of motion without regard to the forces that create it
- Kinematics is important in many instances in Robotics
- The study of dynamics allows us to understand the forces and torques which act on a system and result in motion
- Understanding these motions, and the required forces, is essential for designing these systems



## Dynamic Simulation Software



<http://www.coppeliarobotics.com/>

<http://www.reflexxes.com/>



## Cool Robotics Share



## Cool Robotics Share (II)



Source: Youtube: Wired, How the Tesla Model S is Made



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